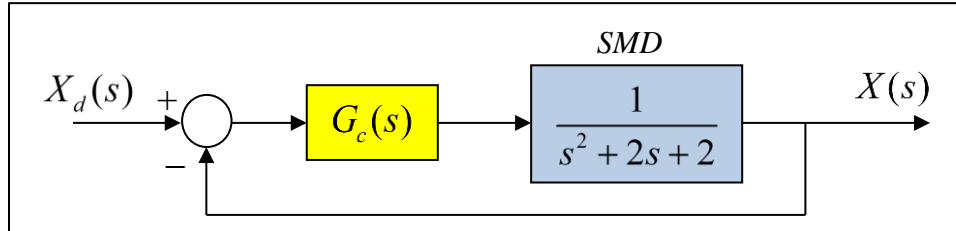


ME 4710 Motion and Control

Frequency Response Design of a Phase-Lead Compensator for a Spring-Mass-Damper (SMD) Positioning System

To illustrate the *frequency response design* of a *phase-lead compensator*, consider the following SMD positioning system controlled by the compensator $G_c(s)$. Here, $X_d(s)$ and $X(s)$ are the *desired* and *actual positions* of the mass.



Using proportional control ($G_c(s) = K$), *large gains* are required to control steady-state error of a step response. Unfortunately, large gains produce *undesirable, oscillatory* closed-loop response. Below, a *phase-lead* compensator is designed to control the steady-state error and give desirable transient response.

Problem: Design a phase-lead compensator so the closed-loop system has a *steady-state position error* $e_{ss} = 1 - x_{ss} < 0.05$ to a unit step input and a *phase margin* $PM = 45$ (deg). Plot the step response of the resulting closed-loop system.

Frequency Response Design

Step 1: Determine the *required compensator gain* to satisfy the *error specification*.

The *steady state error* can be defined in terms of the loop transfer function as

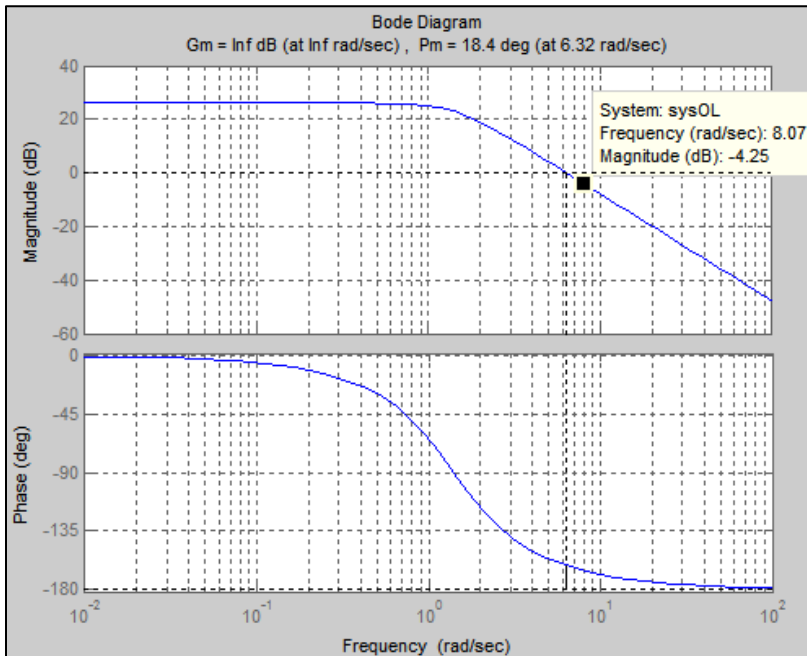
$$e_{ss} = \lim_{s \rightarrow 0} \left[\frac{1}{1 + GH(s)} \right] = \frac{1}{1 + K/2} = \frac{1}{1 + K_p} < 0.05$$

To satisfy this specification, $K_p > 19$ and $K > 38$. $K = 40$ is used below as a starting value.

Step 2: Evaluate the *phase margin* of the *uncompensated system*.

Using MATLAB, the phase margin of this (the *uncompensated* system) is $PM \cong 18.4$ (deg).

This is obviously *well below* the *desired* phase margin. See plot below.



Phase Margin of the Uncompensated System is 18.4 (deg)

Step 3: Calculate the ratio $\alpha = p/z$

An **additional 27 degrees of phase margin** are required, so the required value of α is

$$\alpha = \frac{1 + \sin(\phi_m)}{1 - \sin(\phi_m)} = \frac{1 + \sin(27)}{1 - \sin(27)} = 2.663$$

Step 4: Find ω_m on the Bode diagram of the uncompensated system

The magnitude $-10\log(\alpha) = -4.254$ (db) occurs at approximately 8 (rad/sec). (See plot above.) So, set $\omega_m \cong 8$ (rad/sec), $p = \omega_m \sqrt{\alpha} \approx 13.06$, and $z = p/\alpha \approx 4.9$. The resulting compensator after the first iteration is

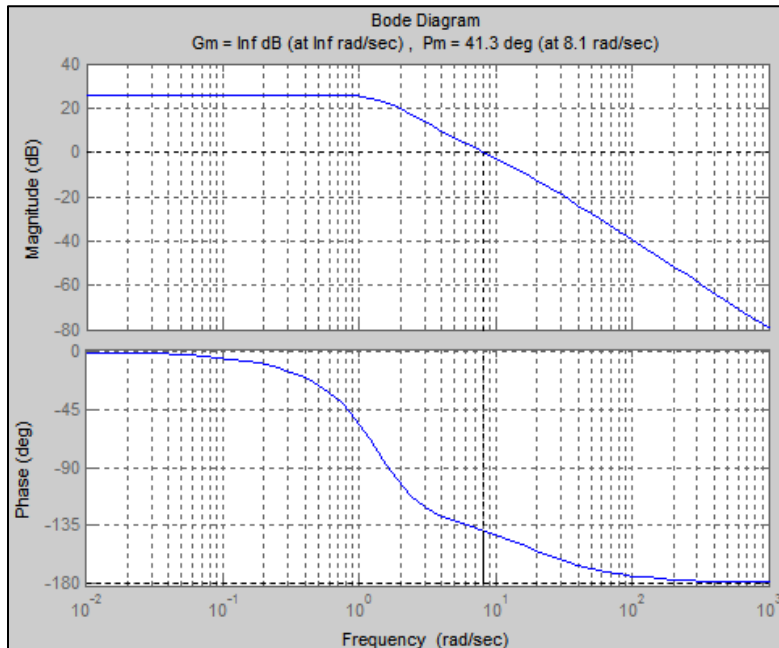
$$G_c(s) = 2.663 \left[\frac{s + 4.9}{s + 13.06} \right] \quad (\text{phase-lead compensator})$$

Step 5: Check the phase margin of the **new compensated system**.

The Bode diagram of the loop transfer function of the compensated system with

$$GH(s) = 2.663 \left[\frac{s + 4.9}{s + 13.06} \right] \left[\frac{40}{s^2 + 2s + 2} \right]$$

shows that the phase margin is $PM = 41.3$ (deg). See plot below.



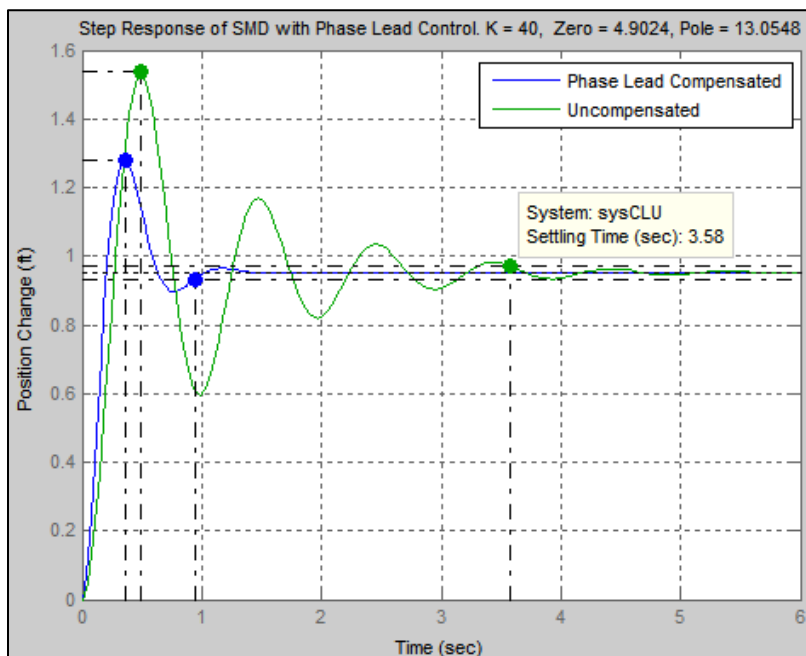
Phase Margin of Compensated System is 41.3 (deg)

Step 6: Repeat steps 3-5 until the desired phase margin is obtained.

If a larger phase margin is desired, steps 3-5 above can be repeated using a desired additional phase margin of higher than 27 degrees. For this example, the above values are used below to check the step response.

Step 7: Check the step response.

The step response of the uncompensated system shows a large overshoot (over 60%) and low damping (settling time of 3.58 (sec)), while the step response of the compensated system shows a smaller overshoot (around 35%) with higher damping (settling time of 0.94 (sec)).



Step response of the compensated system is much better than the uncompensated system. **Try increasing the phase margin to get a better response.**

Settling times:
 Uncompensated = 3.58 (sec)
 Compensated = 0.94 (sec)

Frequency Response of Compensated Closed Loop System:

The frequency response of the closed loop system is shown below. The ***bandwidth*** of the closed loop system is approximately 13 (rad/s).

