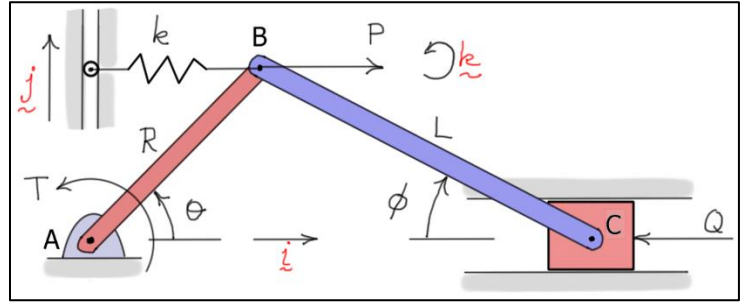


## ME 5550 Intermediate Dynamics

### Principle of Virtual Work – Example

The figure shows a *slider crank mechanism* with zero offset under the action of an *external torque*  $T$  acting on link  $AB$ , *external forces*  $P$  and  $Q$  acting at  $B$  and  $C$ , and a *linear spring* attached at  $B$ .



Problem: *Given* values for  $T$  and  $P$  and that the spring has unstretched length  $\ell_u$ , *find* the force  $Q$  required to hold the mechanism in *equilibrium* at some angle  $\theta$ .

Solution: (using  $\theta$  as the *generalized coordinate*)

Generalized Force (using some partial velocities from previous notes)

The *generalized force* associated with  $\theta$  is: 
$$F_\theta = (F_\theta)_P + (F_\theta)_Q + (F_\theta)_{spring} + (F_\theta)_T$$

- $(F_\theta)_P = (P\mathbf{i}) \cdot \left( \frac{\partial \mathbf{v}_B}{\partial \dot{\theta}} \right) = (P\mathbf{i}) \cdot \frac{\partial}{\partial \dot{\theta}} (R\dot{\theta}(-S_\theta\mathbf{i} + C_\theta\mathbf{j})) = (P\mathbf{i}) \cdot (R(-S_\theta\mathbf{i} + C_\theta\mathbf{j})) = \boxed{-PRS_\theta}$
- $(F_\theta)_{spring} = (-f_{sp}\mathbf{i}) \cdot \left( \frac{\partial \mathbf{v}_B}{\partial \dot{\theta}} \right) = (-f_{sp}\mathbf{i}) \cdot (R(-S_\theta\mathbf{i} + C_\theta\mathbf{j})) = f_{sp}RS_\theta = \boxed{k(RC_\theta - \ell_u)RS_\theta}$
- $(F_\theta)_Q = (-Q\mathbf{i}) \cdot \left( \frac{\partial \mathbf{v}_C}{\partial \dot{\theta}} \right) = (-Q\mathbf{i}) \cdot [-R(S_\theta + C_\theta S_\phi / C_\phi)\mathbf{i}] = \boxed{QR(S_\theta + C_\theta S_\phi / C_\phi)}$
- $(F_\theta)_T = (T\mathbf{k}) \cdot \left( \frac{\partial \dot{\theta}}{\partial \dot{\theta}} \right) = T\mathbf{k} \cdot \mathbf{k} = \boxed{T}$

### Principle of Virtual Work

Applying the *principle of virtual work* and solving for the force  $Q$  gives

$$F_\theta = 0 = -PRS_\theta + k(RC_\theta - \ell_u)RS_\theta + QR(S_\theta + C_\theta S_\phi / C_\phi) + T$$

$$\Rightarrow \boxed{Q = \frac{PRS_\theta - k(RC_\theta - \ell_u)RS_\theta - T}{R(S_\theta + C_\theta S_\phi / C_\phi)}}$$

Notes:

1. The *pin forces* at  $A$ ,  $B$ , and  $C$  and the *normal force* at  $C$  are inactive (have no contribution).
2. The forces and torques that contribute to  $F_\theta$  are *active*.
3. There is only *one equation* associated with the one degree-of-freedom of the system.
4. The contribution of the spring could be calculated using *potential energy*.