

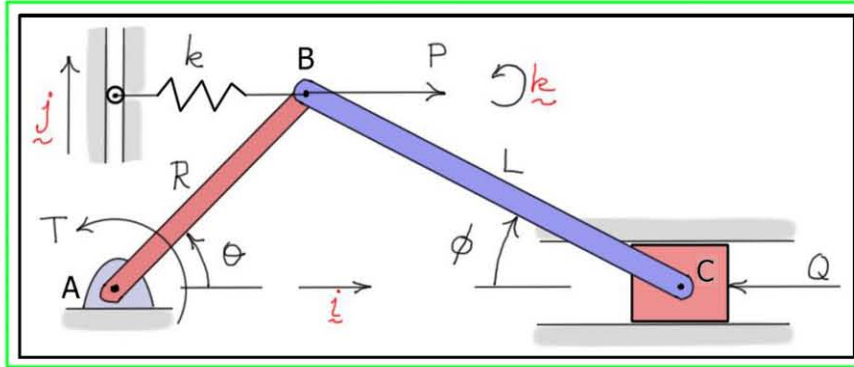
## Example #18 – Intermediate Dynamics: Principle of Virtual Work

Active Forces/Torques:

- $P, Q, T$  (neglecting weight forces)
- spring (unstretched length,  $\ell_u$ )

Find:

- Force  $Q$  required to hold the system in equilibrium at some angle  $\theta$



Solution: (using  $\theta$  as the generalized coordinate)

For equilibrium of this system, the *principle of virtual work* states

$$F_\theta = (F_\theta)_P + (F_\theta)_Q + (F_\theta)_{spring} + (F_\theta)_T = 0$$

Here,

$$(F_\theta)_P = (P\mathbf{i}) \cdot \left( \frac{\partial \mathbf{v}_B}{\partial \dot{\theta}} \right) = (P\mathbf{i}) \cdot \frac{\partial}{\partial \dot{\theta}} (R\dot{\theta}(-S_\theta\mathbf{i} + C_\theta\mathbf{j})) = (P\mathbf{i}) \cdot (R(-S_\theta\mathbf{i} + C_\theta\mathbf{j})) = \boxed{-PRS_\theta}$$

$$(F_\theta)_{spring} = (-f_{sp}\mathbf{i}) \cdot \left( \frac{\partial \mathbf{v}_B}{\partial \dot{\theta}} \right) = (-f_{sp}\mathbf{i}) \cdot (R(-S_\theta\mathbf{i} + C_\theta\mathbf{j})) = f_{sp}RS_\theta = \boxed{k(RC_\theta - \ell_u)RS_\theta}$$

$$(F_\theta)_Q = (-Q\mathbf{i}) \cdot \left( \frac{\partial \mathbf{v}_C}{\partial \dot{\theta}} \right) = (-Q\mathbf{i}) \cdot [-R(S_\theta + C_\theta S_\phi/C_\phi)\mathbf{i}] = \boxed{QR(S_\theta + C_\theta S_\phi/C_\phi)}$$

$$(F_\theta)_T = (T\mathbf{k}) \cdot \left( \frac{\partial \omega_{AB}}{\partial \dot{\theta}} \right) = T\mathbf{k} \cdot \mathbf{k} = \boxed{T}$$

Substituting into the principle of virtual work and solving for  $Q$  gives

$$F_\theta = 0 = -PRS_\theta + k(RC_\theta - \ell_u)RS_\theta + QR(S_\theta + C_\theta S_\phi/C_\phi) + T$$

$$\Rightarrow \boxed{Q = \frac{PRS_\theta - k(RC_\theta - \ell_u)RS_\theta - T}{R(S_\theta + C_\theta S_\phi/C_\phi)}}$$

Notes:

- Pin forces at  $A, B$ , and  $C$  and normal force at  $C$  do not contribute to  $F_\theta$  (“*non-active*”)
- Forces and torques that contribute to  $F_\theta$  are said to be “*active*”
- There is only *one equation* associated with the *degree-of-freedom* of the system.
- The *choice* of generalized coordinate is ours.
- The contribution of the spring could be calculated using *potential energy*.

$$(F_\theta)_{spring} = -\frac{\partial V_{sp}}{\partial \theta} = -\frac{\partial}{\partial \theta} \left( \frac{1}{2} k e^2 \right) = -\frac{1}{2} k \frac{\partial}{\partial \theta} (RC_\theta - \ell_u)^2 = \boxed{k(RC_\theta - \ell_u)RS_\theta}$$