

Intermediate Dynamics: Thrust Bearing Example

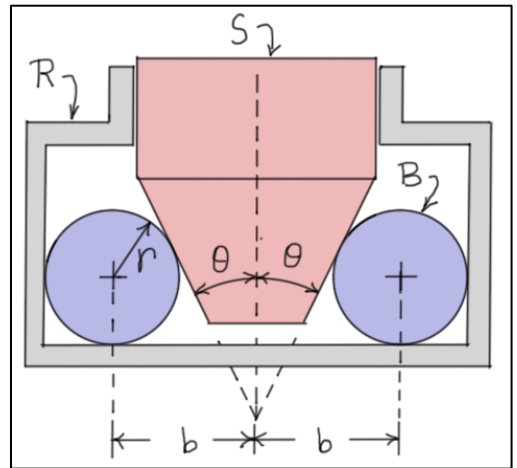
(Reference: Kane and Levinson, *Dynamics: Theory and Applications*, McGraw-Hill, 1985.)

Problem:

Given the thrust bearing in the diagram, show that for **pure rolling** between the shaft S and the bearing B , it is

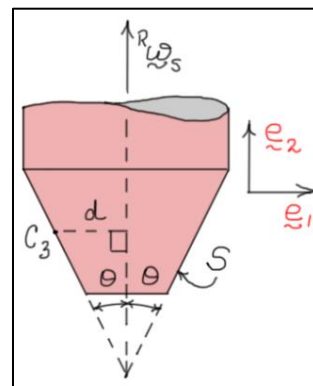
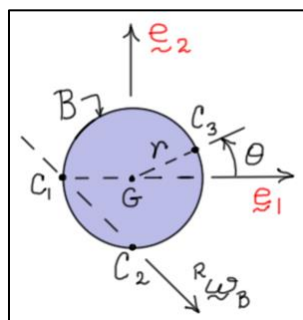
required that $b = \frac{r(1 + S_\theta)}{C_\theta - S_\theta}$. Note that **pure rolling** occurs

between S and B if **no slipping** occurs and if ${}^B\omega_S$ the angular velocity of the shaft (S) relative to the bearing (B) is **parallel** to the **common tangent plane** between S and B . Assume also that **no slip** occurs between the bearing and the race (R).



Solution:

1. Consider the separate diagrams below of the shaft and the bearing. Points C_1 and C_2 represent the contact points between the bearing and the race (R), and C_3 represents the contact point between the shaft and the bearing. The unit vectors \underline{e}_1 and \underline{e}_2 represent the horizontal and vertical directions in the plane defined by these three points. To complete the unit vector set, a third unit vector is defined as $\underline{e}_3 = \underline{e}_1 \times \underline{e}_2$.



Given this set-up and the **no-slip conditions** at points C_1 , C_2 , and C_3 , the angular velocities of the shaft and the bearing may be written as

$$\boxed{{}^R\omega_S = {}^R\omega_S \underline{e}_2} \quad \boxed{{}^R\omega_B = {}^R\omega_B \left(\frac{\sqrt{2}}{2} \underline{e}_1 - \frac{\sqrt{2}}{2} \underline{e}_2 \right)} \quad (1)$$

2. The **angular velocities** of the shaft and the bearing in R can be **related** by calculating the velocity of the contact point C_3 . In this process, advantage is taken of the fact that the velocities of the points C_1 and C_2 relative to R are zero due to the **no-slip** condition.

$$\begin{aligned}
{}^R \mathcal{V}_{C_3} &= {}^R \mathcal{V}_{C_1} + {}^R \mathcal{V}_{C_3/C_1} = 0 + ({}^R \omega_B \times \mathcal{L}_{C_3/C_1}) \\
&= {}^R \omega_B \left(\frac{\sqrt{2}}{2} \mathbf{e}_1 - \frac{\sqrt{2}}{2} \mathbf{e}_2 \right) \times (r(1 + C_\theta) \mathbf{e}_1 + rS_\theta \mathbf{e}_2) \quad (C_3 \text{ is a point on the } \mathbf{bearing}) \\
\Rightarrow & \boxed{{}^R \mathcal{V}_{C_3} = \frac{\sqrt{2}}{2} r (S_\theta + (1 + C_\theta)) {}^R \omega_B \mathbf{e}_3}
\end{aligned}$$

Also,

$$\boxed{{}^R \mathcal{V}_{C_3} = d {}^R \omega_S \mathbf{e}_3 = (b - rC_\theta) {}^R \omega_S \mathbf{e}_3} \quad (C_3 \text{ is a point on the } \mathbf{shaft})$$

Assuming there is *no-slip* between the *bearing* and the *shaft*, these two velocities must be equal. Setting the two equal leads to the conclusion that

$$\boxed{{}^R \omega_S = \frac{\sqrt{2}}{2} \left[\frac{r(1 + S_\theta + C_\theta)}{(b - rC_\theta)} \right] {}^R \omega_B} \quad (2)$$

3. The *angular velocities* of the shaft and the bearing can also be related using the *summation rule* for angular velocities. That is,

$$\boxed{{}^R \omega_S = {}^R \omega_B + {}^B \omega_S} \quad (3)$$

Here, ${}^R \omega_B$ the angular velocity of the bearing is given by Eq. (1), ${}^R \omega_S$ the angular velocity of the shaft is given by Eqs. (1) and (2), and for *pure rolling* between *S* and *B*,

$$\boxed{{}^B \omega_S = {}^B \omega_S (-S_\theta \mathbf{e}_1 + C_\theta \mathbf{e}_2)} \quad (4)$$

Substituting from Eqs. (1), (2), and (4) into Eq. (3) gives the following two scalar equations.

$$\boxed{
\begin{aligned}
\frac{\sqrt{2}}{2} {}^R \omega_B - S_\theta {}^B \omega_S &= 0 \\
-\frac{\sqrt{2}}{2} {}^R \omega_B + C_\theta {}^B \omega_S &= \frac{\sqrt{2}}{2} \left[\frac{r(1 + S_\theta + C_\theta)}{(b - rC_\theta)} \right] {}^R \omega_B
\end{aligned}
} \quad (5)$$

Multiplying the first equation by C_θ and the second by S_θ , adding the two equations, and simplifying gives the desired result.

$$\boxed{b = \frac{r(1 + S_\theta)}{C_\theta - S_\theta}}$$